# ASCO Power Technologies <br> Engineering Application Information 

## WITHSTAND AND CLOSING RATINGS

FOR
TRANSFER SWITCH EQUIPMENT

ASCO products comply with all mandatory UL 1008 withstand and closing ratings.

By using the information in this publication and calculating available short circuit currents, the system designer can be assured the transfer switches will be properly rated for the electrical system.

## Guidelines for using the information in this publication to verify suitability of switches for specific applications based on withstand current ratings

1. Determine the prospective fault current available (from each source) at the location of the switch.
2. Determine the overcurrent protective devices (OPDs) that will be located ahead of the switch.
3. If the OPD is a circuit breaker, refer to Table II on page 3. Select the switch rating necessary to handle the full load current. Compare the fault current available at the switch to the withstand current rating (WCR) shown in Table II for the applicable switch ampere size and voltage. If the prospective fault current is equal to or less than the WCR from Table II, the switch selected is suitable for the application.
4. If the prospective fault current is greater than the WCR obtained from Table II, refer to Table III on pages 3-7. Compare the fault current to the WCR shown in Table III. If the fault current is equal to or less than the WCR shown in Table III, the switch is suitable for the application when protected by any of the circuit breakers shown. If the specific circuit breaker being used is not shown in the table, contact ASCO Power Technologies.
5. If the prospective fault current is greater than the WCR listed in Table III, refer to Special Application Considerations on page 8.
6. When the overcurrent protective devices are current limiting fuses refer to Table II on page 3. If there are any questions about the suitability of the switch when protected by current limiting fuses contact ASCO Power Technologies.

## Introduction

This publication provides information on withstand current ratings (WCRs) for ASCO transfer switches and related products, including compliance with the optional $1 \frac{1}{2}$ and 3 cycle "any breaker" WCRs and other revisions to UL 1008. Also included are guidelines for special WCR applications and typical methods for specifying WCR requirements.

## The Importance of Proper Ratings

The transfer switch is a unique and critical part of the power system. It is the last distribution device feeding the critical loads of a facility. For that reason, the transfer switch should be located as close as possible to the protected loads. In addition, after a fault (short circuit) is cleared, the transfer switch must remain operable so that it can restore power to the critical loads from the alternate power source.
In the design of an electrical power distribution system, a coordination study should be conducted to determine the trip settings required for all circuit breakers. Proper trip settings will assure that a fault is cleared as close to its location as practical. The coordination study considers conductor sizes, quantities and lengths as well as any other relevant circuit impedance. The farther from the source a device is located, the lower the fault current will be. Referring to Figure 1, a fault at point A should be cleared by the switchgear feeder breaker $\mathrm{F}_{2}$ and not by M. This would leave the other feeder circuits ( $\mathrm{F}_{1} \& \mathrm{~F}_{3}-\mathrm{F}_{7}$ ) in operation. A coordination study will determine the magnitude of fault current at the load side of the transfer switch and indicate the settings for $\mathrm{F}_{2}$.

Consider a fault at point B on the load side of the breaker feeding $L_{1}$ as shown in Figure 1. If the system


Figure 1. Line diagram of a typical emergency power system.
breakers have been coordinated properly, the breaker feeding $L_{1}$ will trip before the upstream breaker or fuse. The transfer switch must withstand this fault current until the circuit breaker or fuse clears the fault. Most automatic transfer switches available today have a standard control circuit time delay of 0.5 seconds or more to override any momentary voltage transients. This is ample time for any over current device to clear the fault, allowing system voltage to return to normal and avoiding any unnecessary operation of the transfer switch.

Now consider a fault at point A of Figure 1. The circuit breakers on the load side of the transfer switch would not see the fault current, but the upstream breaker (F2) would and the instantaneous trip element would be actuated. The transfer switch controller senses there is no voltage from the utility, signals a transfer operation and the transfer switch is now required to close on the fault condition until the generator over current device clears the fault.

If a transfer switch does not have a sufficient with-stand current rating, severe damage and a potential fire hazard could result from the fault current. Over-rating the transfer switch to achieve a sufficient withstand current rating leads to a less cost-effective design. Good engineering practice requires adequately rated devices in the power distribution system. Therefore, the specified WCR for the transfer switch should be the available fault current at the location of the transfer switch. Some recommended engineering practices to assist in fault current calculations are referenced at the end of this publication.

## How Codes Impact Ratings

Codes often require equipment to be approved for its intended use. For example, one of the most common applications for automatic transfer switches is in Emergency Systems per Article 700 of the National Electrical Code (NEC) ANSI/NFPA 70. Section 700-3 and $700-6$ require that all transfer equipment be approved for use on Emergency Systems. How does a manufacturer obtain approval? There are several ways, but perhaps the most common is via a third party certification acceptable to the authority having jurisdiction.

## The Role of Underwriters Laboratories

Underwriters Laboratories (UL) is one of several independent testing agencies and is perhaps the most well-known third party certifier. The Standard for Safety under which Underwriters Laboratories tests Transfer Switch Equipment is UL 1008. Equipment which meets UL requirements is listed in UL's Electrical Construction Materials List. This list is frequently used by electrical inspectors and other authorities having
jurisdiction in conjunction with the device markings and rating label to approve an electrical installation.

UL has issued several revisions to the UL 1008 Standard, which redefine how a transfer switch is to be tested and marked for fault current withstand and closing ratings. A major revision introduced in the 1989 version of UL 1008 allowed an optional rating category for WCR and closing tests. Its purpose was to permit transfer switch manufacturers to conduct tests without overcurrent protective devices. For transfer switches rated 400 A and below for use on 10 kA circuit maximum, the on time of the fault current must be at least 25 ms ( $11 / 2$ cycles). For transfer switches rated above 400 A or for use on circuits with available fault currents above 10 kA , the on time of the fault current must be at least 50 ms ( 3 cycles). When this test is successful, the manufacturer may mark the switch for use with any manufacturer's circuit breaker within its rating. Such umbrella ratings give the application engineer more flexibility when specifying and coordinating the transfer switch with overcurrent devices.

Where a transfer switch manufacturer does not opt for this test, the switch can only be marked to show the specific manufacturer's circuit breaker with which the switch was tested, or circuit breakers approved by UL through extension from the original test data. The specific breaker marking can limit the product's application and acceptance by the inspecting authority.

Other issues may develop when the transfer switch WCR is limited to use with specific circuit breakers. Even though a specific breaker is coordinated with the transfer switch upon initial installation, the breaker could possibly be replaced at a later date with another type and/or rating which is not one of the breakers approved by UL. Circuit breakers also change trip characteristics as they age and the tripping time may be become slower, allowing the transfer switch to be subjected to energy above the original short circuit testing values. These issues would not be a concern to the specifying engineer if a transfer switch rated for use with "any breaker" were selected.

## ASCO Switches Meet and Exceed UL 1008 Requirements

ASCO Power Technologies provides withstand current ratings on its products to provide maximum flexibility to the electrical consultant when specifying these products. The ratings apply to the ASCO products shown in Table I and are specified in Tables II and III. The ratings apply to single phase and three phase switches. The withstand current ratings of the overlapping neutral transfer pole is identical to the WCR of the phase switching poles.
See page 6, Special Application Considerations, if ratings beyond those listed are required. Contact ASCO Power Technologies to determine if ratings have been increased or for ratings beyond three cycles which may not be UL Listed, but which are based on other tests.

Table I. Applicable Products (Refer to Specific Rating Tables for Each Products Rating)

| ASCO <br> Product | Typical Applications | Product Description |  |
| :---: | :---: | :---: | :---: |
|  |  | Automatic Transfer Switch | Non-Automatic Transfer Switch |
| Series 165 | Residential | Automatic | Manual |
| $\begin{aligned} & \text { Series } 300 \text { / } \\ & 386 \end{aligned}$ | Industrial / Light Commercial | Automatic Transfer Switch (Light Commercial Applications) | Non-Automatic - Electrically Operated Transfer Switch |
| 4000 TS 4000 Series Power Transfer Switches | Industrial, Commercial, Institutional | 4ATS - Automatic Transfer Switch <br> 4ACTS - Automatic Closed Transition Switch <br> 4ADTS - Automatic Delayed Transition Switch | 4NTS - Non-Automatic Transfer Switch 4NCTS - Non-Automatic Closed Transition Switch 4NDTS - Non-Automatic Delayed Transition Switch |
| 7000 TS <br> 7000 Series <br> Power <br> Transfer <br> Switches | Health Care, Critical Power Facilities | 7ATS - Automatic Transfer Switch 7ACTS - Automatic Closed Transition Switch 7ADTS - Automatic Delayed Transition Switch 7ASLS - Automatic Soft Load Transfer Switch | 7NTS - Non-Automatic Transfer Switch 7NCTS - Non-Automatic Closed Transition Switch 7NDTS - Non-Automatic Delayed Transition Switch 7MTS - Manually Operated Transfer Switch |
| 7000 TB <br> 7000 Series <br> Transfer <br> Switches <br> with Bypass- <br> Isolation <br> Feature | Health Care, Critical Power Facilities, Mission Critical | 7ATB - Automatic Transfer Switch with Bypass-Isolation <br> 7ACTB - Automatic Closed Transition Transfer Switch with Bypass-Isolation <br> 7ADTB - Automatic Delayed Transition <br> Transfer Switch with Bypass-Isolation <br> 7ASLB - Automatic Soft Load Transfer Switch with Bypass-Isolation | 7NTB - Non-Automatic Transfer Switch with Bypass-Isolation <br> 7NCTB - Non-Automatic Closed Transition Transfer Switch with Bypass-Isolation 7NDTB - Non-Automatic Delayed Transition Transfer Switch with Bypass-Isolation |

Table II. Withstand / Closing Ratings for ASCO Transfer Switches
Used with "Any Circuit Breaker"1 or Current Limiting Fuses

| ASCO <br> Transfer Switch Product | Transfer Switch Frame Prefix | Transfer Switch Rating (amps) | Withstand / Closing Ratings (RMS Symmetrical Amps) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | When Protected With Any Circuit Breaker |  |  | When Protected With Current Limiting Fuses |  |  |  |
|  |  |  | Volts max. | $\begin{gathered} \text { KA } \\ \text { max. } \end{gathered}$ | Time Cycles <br> @ 60Hz | kA | Volts max. | Max. Fuse Size (amps) | Fuse Class |
| 165 TS | D | 100, 200, 230 | 240 | 10 | 1.5 |  |  | - |  |
| 4000 TS <br> 7000 TS 4ATS, 7ATS 4NTS, 7NTS 7MTS | D | 30 | 600 | 10 | 1.5 | 100 |  | 60 |  |
|  |  | 70, 100, 125, 150 |  |  |  |  |  |  |  |
|  |  | 200 | 480 |  |  | 200 | 480 | 200 | J |
|  |  | 230 |  |  |  | 100 |  | 300 |  |
|  | J | $150{ }^{2}, 260,400,600^{2}$ | 600 | 35 | 3 | 200 | 600 | 600 |  |
|  |  |  | 240 | 65 |  |  |  | 800 |  |
|  | H | 800, 1000, 1200 | 600 | 50 |  |  |  |  | L |
|  |  |  |  | 36 | 18 |  |  |  |  |
| 7000 TB | E | 150 | 480 | 35 | 3 | 200 | 480 | 450 | J |
|  |  | 150 | 600 | 22 |  |  |  |  |  |
|  |  | 260, 400 | 480 | 35 |  |  |  | 600 |  |
|  | H | 600, 800, 1000, 1200 | 600 | 50 36 | 18 |  | 600 | 1600 | L |
| 4000 TS 7000 TS 7000 TB | G | 1600, 2000 front connected | 600 | 85 | 3 | 200 | 600 |  | L |
|  |  | 1600, 2000 |  | 100 |  |  |  |  |  |
|  |  | 2600, 3000 |  |  |  |  |  | 4000 |  |
|  | E | 4000 |  | 100 |  |  | 480 | 6000 |  |

${ }^{1}$ Any breaker ratings based on 3 cycle duration for 260-4000 amp continuous ratings and 1-1/2 cycles for 30-230 amp.
${ }^{2} \mathrm{~J} 150$ amp is 4ACTS, 4ADTS, 7ACTS, 7ADTS, \& 7ASLS only.

Table III. Withstand / Closing Ratings for Transfer Switches Used with Specific Manufacturer's Molded Case Circuit Breakers

|  |  |  | Withstand <br> / Closing Rating kA RMS Symmetrical amps | $\begin{aligned} & \dot{㐅} \\ & \stackrel{1}{\omega} \\ & \stackrel{n}{0} \\ & \stackrel{n}{0} \end{aligned}$ |  | Circuit Breaker Type or Class | Circuit Breaker Rating (amps max.) <br> Per NEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 300 | D | 30 | 10 | 600 | Any | Any Breaker |  |
| $\begin{gathered} 300 \\ 386 \\ 4000 \text { TS } \\ 7000 \text { TS } \end{gathered}$ | D | 70 | 22 | 480 | GE | TB1 | 100 |
|  |  |  |  |  |  | TEL, THED, THLC1, THLC2 | 150 |
|  |  |  |  |  |  | TFL | 225 |
|  |  |  |  |  | I-T-E | CED6, ED6, HED4, HED6 | 125 |
|  |  |  |  |  |  | CFD6 | 150 |
|  |  |  |  |  |  | FD6, FXD6, HFD6 | 250 |
|  |  |  |  |  | Square-D | FH | 80 |
|  |  |  |  |  |  | FC, FI | 100 |
|  |  |  |  |  |  | KA, KC, KH, KI, LA, LH | 250 |
|  |  |  |  |  | CutlerHammer | FCL, TRI-PAC FB | 100 |
|  |  |  |  |  |  | FD, FDC, HFD | 150 |
|  |  |  |  |  |  | HJD, JD, JDB, JDC | 250 |
|  |  |  |  |  |  | HKD, KD, KDB,KDC,LCL, TRI-PAC LA | 400 |
|  |  |  |  |  | ABB | S1 | 125 |
|  |  |  |  |  |  | S3 | 150 |
|  |  |  |  |  | Merlin Gerin | CE104, CE106 | 100 |

Table III. continued

|  |  |  | Withstand <br> / Closing Rating kA RMS <br> Symmetrical amps |  |  | Circuit Breaker <br> Type or Class | Circuit <br> Breaker Rating (amps max.) <br> Per NEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 300 \\ 386 \\ 4000 \text { TS } \\ 7000 \text { TS } \end{gathered}$ | D | 100 | 22 | 480 | GE | TB1 | 100 |
|  |  |  |  |  |  | TEL, THED, THLC1, THLC2 | 150 |
|  |  |  |  |  |  | TFL | 225 |
|  |  |  |  |  | I-T-E | CED6, ED6, HED4, HED6 | 125 |
|  |  |  |  |  |  | CFD6 | 150 |
|  |  |  |  |  |  | FD6, XD6, HLD6 | 250 |
|  |  |  |  |  | Square-D | FC, FI | 100 |
|  |  |  |  |  |  | KA, KC, KH, KI, LA, LH | 250 |
|  |  |  |  |  | CutlerHammer | FCL, TRI-PAC FB | 100 |
|  |  |  |  |  |  | FD, FDC, HFD | 150 |
|  |  |  |  |  |  | HJD, JD, JDB, JDC | 250 |
|  |  |  |  |  |  | HKD, KD, KDB,KDC, LCL, TRI-PAC LA | 400 |
|  |  |  |  |  | ABB | S1 | 125 |
|  |  |  |  |  |  | S3 | 150 |
|  |  |  |  |  | Merlin Gerin | CE104, CE106 | 100 |
|  |  |  |  |  |  | CF250 | 250 |
| $\begin{aligned} & 4000 \text { TS } \\ & 7000 \text { TS } \end{aligned}$ | D | 125 | 22 | 480 | GE | TEL, THED, THLC1 | 150 |
|  |  |  |  |  |  | TFL, THFK, THLC2 | 225 |
|  |  |  |  |  |  | SFL, SFP, TFJ, TFK | 250 |
|  |  |  |  |  |  | SGL4, SGP4, TLB4 | 400 |
|  |  |  |  |  | I-T-E | CFD6 | 200 |
|  |  |  |  |  |  | FD6, FXD6, HFD6 | 250 |
|  |  |  |  |  | Square-D | KA, KC, KH, KI | 250 |
|  |  |  |  |  | CutlerHammer | FD, FDC, HFD | 150 |
|  |  |  |  |  |  | HJD, JD, JDB, JDC | 250 |
|  |  |  |  |  |  | HKD, KD, KDB,KDC,LCL,TRI-PAC LA | 400 |
|  |  |  |  |  | ABB | S3 | 150 |
|  |  |  |  |  | Merlin Gerin | CF250 | 250 |
| $\begin{gathered} 300 \\ 386 \\ 4000 \text { TS } \\ 7000 \text { TS } \end{gathered}$ | D | $\begin{aligned} & 150 \\ & 200 \\ & 230 \end{aligned}$ | 22 | 480 | GE | TEL, THED, THLC1 | 150 |
|  |  |  |  |  |  | TFL, THFK, THLC2 | 225 |
|  |  |  |  |  |  | SFL, SFP, TFJ, TFK | 250 |
|  |  |  |  |  |  | SGL4, SGP4, TLB4 | 400 |
|  |  |  |  |  | I-T-E | CFD6, FD6, FXD6, HFD6 | 250 |
|  |  |  |  |  |  | CJD6, HHJD6, HHJXD6, HJD6, JD6, JXD6, SCJD6 | 400 |
|  |  |  |  |  |  | SHJD6, SJD6 | 400 |
|  |  |  |  |  | Square-D | KA, KC, KH, KI | 250 |
|  |  |  |  |  |  | LC, LI | 300 |
|  |  |  |  |  |  | LA, LH | 400 |
|  |  |  |  |  | CutlerHammer | FD, FDC, HFD | 150 |
|  |  |  |  |  |  | JD, JDB, JDC, HJD | 250 |
|  |  |  |  |  |  | HKD, KD, KDB,KDC,LCL,TRI-PAC LA | 400 |
|  |  |  |  |  | ABB | S3 | 150 |
|  |  |  |  |  | Merlin Gerin | CF250 | 250 |
|  |  |  |  |  |  | CJ400 | 400 |
| 300, 386 4000 TS 7000 TS | D | $\begin{aligned} & 150 \\ & 200 \\ & 230 \end{aligned}$ | 42 | 240 | Square-D | JG | 250 |
| 7000 TB | E | 150 | 42 | 480 | GE | TEL, THED, THLC1 | 150 |
|  |  |  |  |  |  | TFL, THLC2 | 225 |
|  |  |  |  |  |  | SFL, SFLA, SFP | 250 |
|  |  |  |  |  |  | SGL4, SGP4, TB4, THLC4, TLB4 | 400 |
|  |  |  |  |  |  | SGLA, SGL6, SGP6, TB6 | 600 |
|  |  |  |  |  | I-T-E | CFD6, HFD6 | 250 |
|  |  |  |  |  |  | CJD6, HHJD6, HHJXD6, HJD6, SCJD6, SHJD6 | 400 |
|  |  |  |  |  |  | CLD6, HHLD6, HHLXD6, HLD6, SHLD6 | 600 |
|  |  |  |  |  | Square-D | KC, KI | 250 |
|  |  |  |  |  |  | LC, LI | 400 |
|  |  |  |  |  | CutlerHammer | HJD, JDC | 250 |
|  |  |  |  |  |  | HKD, KDC, LCL, TRI-PAC LA | 400 |
|  |  |  |  |  |  | HLD | 600 |
|  |  |  |  |  |  | TRI-PAC NB | 800 |
|  |  |  |  |  | ABB | S3 | 150 |
|  |  |  |  |  | Merlin Gerin | CF250 | 250 |
|  |  |  |  |  |  | CJ400 | 400 |

Table III. continued

|  |  |  | Withstand <br> / Closing Rating <br> kA RMS <br> Symmetrical amps | $\begin{aligned} & \dot{\text { 㐅}} \\ & \text { ■ } \\ & \text { n } \\ & \stackrel{\#}{0} \end{aligned}$ |  | Circuit Breaker <br> Type or Class | Circuit <br> Breaker Rating (amps max.) <br> Per NEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4000 CTS 4000 DTS 7000 CTS 7000 DTS | J | 150 | 50 | 480 | CutlerHammer | HJD, JDC, JGH, JGC | 250 |
|  |  |  |  |  |  | HKD, CHKD, KDC | 400 |
|  |  |  |  |  |  | HLD, CHLD, LDC, CLDC | 600 |
|  |  |  |  |  | GE | SFL, SFP | 250 |
|  |  |  |  |  |  | TJL4V, TJL1S-6S | 600 |
|  |  |  |  |  |  | SGL1, SGL4, SGP1, SGP4 | 600 |
|  |  |  |  |  | Siemens | HFD, HFXD | 250 |
|  |  |  |  |  |  | HJD, HJXD, SHJD | 400 |
|  |  |  |  |  | Square-D | KC | 250 |
|  |  |  |  |  |  | CK400N, CK400NN, CM1250HH | 400 |
|  |  |  | 42 | 600 | CutlerHammer | JGC | 250 |
|  |  |  |  |  |  | KDC | 400 |
|  |  |  |  |  |  | LDC, CLDC | 600 |
|  |  |  |  |  | GE | SGL1, SGL4, SGP1, SGP4 | 600 |
| $\begin{gathered} 300 \\ 386 \\ 7000 \mathrm{~TB} \end{gathered}$ | E | 260 | 42 | 480 | GE | TFL, THLC2 | 225 |
|  |  |  |  |  |  | SFL, SFLA, SFP | 250 |
|  |  |  |  |  |  | SGL4, SGP4, TB4, THLC4, TLB4 | 400 |
|  |  |  |  |  |  | SGLA, SGL6, SGP6, TB6 | 600 |
|  |  |  |  |  |  | SKHA, SKLB, SKP8, TKL | 800 |
|  |  |  |  |  | I-T-E | CFD6, FD6, FXD6, | 250 |
|  |  |  |  |  |  | CJD6, HHJD6, HHJXD6, HJD6, JD6, JXD6, SCJD6 | 400 |
|  |  |  |  |  |  | SHJD6, SJD6 | 400 |
|  |  |  |  |  |  | CLD6, HHLD6, HHLXD6, HLD6, SCLD6, SHLD6 | 600 |
|  |  |  |  |  |  | CMD6, HMD6, HND6, MD6, MXD6, SCMD6, SHMD6 | 800 |
|  |  |  |  |  |  | SMD6, SND6 | 800 |
|  |  |  |  |  | Square-D | KC, KI | 250 |
|  |  |  |  |  |  | LC,LI | 600 |
|  |  |  |  |  |  | MH | 800 |
|  |  |  |  |  | CutlerHammer | HJD, JDC | 250 |
|  |  |  |  |  |  | HKD, KDC, LCL, TRI-PAC LA | 400 |
|  |  |  |  |  |  | HLD | 600 |
|  |  |  |  |  |  | TRI-PAC NB | 800 |
|  |  |  |  |  | ABB | S5 | 400 |
|  |  |  |  |  |  | 56 | 800 |
|  |  |  |  |  | Merlin Gerin | CF250 | 250 |
|  |  |  |  |  |  | CJ400 | 400 |
| $\begin{aligned} & 4000 \text { TS } \\ & 7000 \text { TS } \end{aligned}$ | J | 260 | 50 | 480 | CutlerHammer | HJD, JDC, JGH, JGC | 250 |
|  |  |  |  |  |  | HKD, CHKD, KDC | 400 |
|  |  |  |  |  |  | HLD, CHLD, LDC, CLDC | 600 |
|  |  |  |  |  |  | MDL, CMDL, HMDL, CHMDL, NGS, NGH, NGC | 800 |
|  |  |  |  |  | GE | SFL, SFP | 250 |
|  |  |  |  |  |  | TBC4 | 400 |
|  |  |  |  |  |  | TBC6, TJL4V, TJL1S-6S | 600 |
|  |  |  |  |  |  | SGL1, SGL4, SGL6, SGP1, SGP4, SGP6 | 600 |
|  |  |  |  |  |  | TBC8, TKL4V, TKH8S-12S, TKL8S-12S | 800 |
|  |  |  |  |  |  | SKH8, SKL8, SKP8 | 800 |
|  |  |  |  |  | Siemens | HFD, HFXD | 250 |
|  |  |  |  |  |  | HJD, HJXD, SHJD | 400 |
|  |  |  |  |  |  | HLD, HLXD, SHLD | 600 |
|  |  |  |  |  |  | LMD, LMXD, HLMD, HLMXD, HMG | 800 |
|  |  |  |  |  |  | MD, MXD, HMD, HMXD, SMD, SHMD | 800 |
|  |  |  |  |  | Square-D | KC | 250 |
|  |  |  |  |  |  | CK400N, CK400NN, CM1250HH | 400 |
|  |  |  |  |  |  | LC | 600 |
|  |  |  |  |  |  | CK800N, CK800NN, CM1600HH | 800 |
|  |  |  | 42 | 600 | CutlerHammer | HJD, JGC | 250 |
|  |  |  |  |  |  | KDC | 400 |
|  |  |  |  |  |  | LDC, CLDC | 600 |
|  |  |  |  |  | GE | TBC4 | 400 |
|  |  |  |  |  |  | TBC6, SGL1, SGL4, SGL6, SGP1, SGP4, SGP6 | 600 |
|  |  |  |  |  |  | TBC8, TKL4V, TKL8S-12S, SKL8, SKP8 | 800 |
|  |  |  |  |  | Siemens | HLMD, HLMXD, HMD, HMXD, SHMD | 800 |

Table III. continued

|  |  |  | Withstand <br> / Closing Rating kA RMS Symmetrical amps | $\begin{aligned} & \dot{\text { 夭 }} \\ & \text { E } \\ & \text { n } \\ & \stackrel{\#}{0} \end{aligned}$ |  | Circuit Breaker <br> Type or Class | Circuit <br> Breaker <br> Rating <br> (amps <br> max.) <br> Per NEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & 4000 \text { TS } \\ & 7000 \text { TS } \end{aligned}$ | J | 400 | 50 | 480 | CutlerHammer | HKD, CHKD, KDC | 400 |
|  |  |  |  |  |  | HLD, CHLD, LDC, CLDC | 600 |
|  |  |  |  |  |  | MDL, CMDL, HMDL, CHMDL, NGS, NGH, NGC | 800 |
|  |  |  |  |  | GE | TBC4 | 400 |
|  |  |  |  |  |  | TBC6, TJL4V, TJL1S-6S | 600 |
|  |  |  |  |  |  | SGL1, SGL4, SGL6, SGP1, SGP4, SGP6 | 600 |
|  |  |  |  |  |  | TBC8, TKL4V, TKH8S-12S, TKL8S-12S | 800 |
|  |  |  |  |  |  | SKH8, SKL8, SKP8 | 800 |
|  |  |  |  |  | Siemens | HJD, HJXD, SHJD | 400 |
|  |  |  |  |  |  | HLD, HLXD, SHLD | 600 |
|  |  |  |  |  |  | LMD, LMXD, HLMD, HLMXD, HMG | 800 |
|  |  |  |  |  |  | MD, MXD, HMD, HMXD, SMD, SHMD | 800 |
|  |  |  |  |  | Square-D | CK400N, CK400NN, CM1250HH | 400 |
|  |  |  |  |  |  | LC | 600 |
|  |  |  |  |  |  | CK800N, CK800NN, CM1600HH | 800 |
|  |  |  | 42 | 600 | CutlerHammer | KDC | 400 |
|  |  |  |  |  |  | LDC, CLDC | 600 |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  | GE | TBC4 | 400 |
|  |  |  |  |  |  | TBC6, SGL1, SGL4, SGL6, SGP1, SGP4, SGP6 | 600 |
|  |  |  |  |  |  | TBC8, TKL4V, TKL8S-12S, SK8L, SK8P | 800 |
|  |  |  |  |  | Siemens | HLMD, HLMXD, HMD, HMXD, SHMD | 800 |
| $\begin{gathered} 300 \\ 386 \\ 7000 \mathrm{~TB} \end{gathered}$ | E | 400 | 42 | 480 | GE | SGL4, SGP4, TB4, THLC4, TLB4 | 400 |
|  |  |  |  |  |  | SGLA, SGL6, SGP6, TB6 | 600 |
|  |  |  |  |  |  | SKHA, SKL8, SKP8, TKL | 800 |
|  |  |  |  |  | I-T-E | CJD6, HHJD6, HHJXD6, HJD6, SCJD6, SHJD6 | 400 |
|  |  |  |  |  |  | CLD6, HHLD6, HHLXD6, HLD6, SCLD6, SHLD6 | 600 |
|  |  |  |  |  |  | CMD6, HMD6, HND6, MD6, MXD6, SCMD6, SHMD6 | 800 |
|  |  |  |  |  |  | SMD6, SND6 | 800 |
|  |  |  |  |  | Square-D | LC, LI | 600 |
|  |  |  |  |  |  | MH | 800 |
|  |  |  |  |  | Cutler- <br> Hammer | HKD, KDC, LCL, TRI-PAC LA | 400 |
|  |  |  |  |  |  | HLD | 600 |
|  |  |  |  |  |  | TRI-PAC NB | 800 |
|  |  |  |  |  | ABB | S5 | 400 |
|  |  |  |  |  |  | S6 | 800 |
|  |  |  |  |  | Merlin Gerin | CJ600 | 600 |

Table III. continued

|  |  |  | Withstand <br> / Closing Rating kA RMS Symmetrical amps | $\begin{aligned} & \dot{\text { ® }} \\ & \text { © } \\ & \text { n } \\ & \stackrel{H}{0} \end{aligned}$ |  | Circuit Breaker <br> Type or Class | Circuit Breaker Rating (amps max.) <br> Per NEC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} 300 \\ 386 \\ 4000 \text { TS } \\ 7000 \text { TS } \end{gathered}$ | J | 600 | 50 | 480 | CutlerHammer | HLD, CHLD, LDC, CLDC | 600 |
|  |  |  |  |  |  | $\begin{aligned} & \text { MDL, CMDL, HMDL, CHMDL, NGS, NGH, } \\ & \text { NGC } \end{aligned}$ | 800 |
|  |  |  |  |  | GE | TBC6, TJL4V, TJL1S-6S | 600 |
|  |  |  |  |  |  | SGL1, SGL4, SGL6, SGP1, SGP4, SGP6 | 600 |
|  |  |  |  |  |  | TBC8, TKL4V, TKH8S-12S, TKL8S-12S | 800 |
|  |  |  |  |  |  | SKH8, SKL8, SKP8 | 800 |
|  |  |  |  |  | Siemens | HLD, HLXD, SHLD | 600 |
|  |  |  |  |  |  | LMD, LMXD, HLMD, HLMXD, HMG | 800 |
|  |  |  |  |  |  | MD, MXD, HMD, HMXD, SMD, SHMD | 800 |
|  |  |  |  |  |  | ND, NXD, HND, HNXD, HNG, SND, SHND | 1200 |
|  |  |  |  |  | Square-D | CK400N, CK400NN, CM1250HH | 400 |
|  |  |  |  |  |  | LC | 600 |
|  |  |  |  |  |  | CK800N, CK800NN, CM1600HH | 800 |
|  |  |  |  |  |  | CM2000HH | 1000 |
|  |  |  |  |  |  | MH, CK1200N, CK1200NN, CM2500HH | 1200 |
|  |  |  | 42 | 600 | CutlerHammer | LDC, CLDC | 600 |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  | GE | TBC6, SGL1, SGL4, SGL6, SGP1, SGP4, SGP6 | 600 |
|  |  |  |  |  |  | TBC8, TKL4V, TKL8S-12S, SKL8, SKP8 | 800 |
|  |  |  |  |  | Siemens | HLMD, HLMXD, HMD, HMXD, SHMD | 800 |
|  |  |  |  |  |  | HND, HNXD, HNG, SHND | 1200 |
| $\begin{gathered} 300 \\ 386 \\ 4000 \text { TS } \\ 7000 \text { TS } \\ 7000 \text { TB } \end{gathered}$ | H | $\begin{array}{r} 600^{4} \\ 800 \\ 1000 \\ 1200 \end{array}$ | 65 | 480 | GE | TB8 | 800 |
|  |  |  |  |  |  | MICROVERSATRIP TKL | 1200 |
|  |  |  |  |  | I-T-E | CLD6, HHLD6, HHLXD6, HLD6, SCLD6, SHLD6 | 600 |
|  |  |  |  |  |  | CMD6, HMD6, SCMD6, SHMD6 | 800 |
|  |  |  |  |  |  | CND6, HND6, SCND6, SHND6 | 1200 |
|  |  |  |  |  |  | CPD6 | 1600 |
|  |  |  |  |  | Square-D | MH SERIES 2 | 1000 |
|  |  |  |  |  |  | SE (LS TRIP), SHE (LS TRIP) | 2500 |
|  |  |  |  | 600 | CutlerHammer | TRI-PAC NB | 800 |
|  |  |  |  |  |  | TRI-PAC PB | 1600 |
|  |  |  |  |  |  | RDC | 2500 |
|  |  |  | 42 | 480 | ABB | S6 | 800 |
|  |  |  |  |  |  | S7 | 1200 |
|  |  |  |  |  | Merlin Gerin | CJ600 | 600 |
|  |  |  |  |  |  | CK1200 | 1200 |

${ }^{4} \mathrm{H} 600 \mathrm{amp}$ is $4000 \mathrm{TS}, 7000 \mathrm{TS} \& 7000$ TB only. Use J 600 amp for Series 300 \& 386.


These are the "any breaker" ratings for the transfer switch. For this switch the rating is 65,000 RMS amps sym-metrical at 240 volts and 35,000 amps at 600 volts.

This area indicates the "specific breaker" ratings, maximum voltage, breaker manufacturer, breaker type, and maximum frame size. This switch is rated either 50,000 or 42,000 RMS amps symmetrical for the specific breakers listed.


There is also a rating when used with current limiting fuses of the Class J maximum size indicated on the label. This switch is rated for 200,000 RMS amps when used witch Class J fuses 600 amps or less.

## Marking Requirements

UL requires markings on each switch listing the approved short circuit ratings for ea ch product and its ampacity. ASCO switches display rating labels similar to the one shown in Figure 2.

## Special Application Considerations

ASCO Power Technologies provides a line of switches which are highly reliable, utilize latest technology, include features most frequently used by the consulting engineer, and which are rated to meet a wide variety of requirements. For special applications, such as when higher ratings or longer withstand times are needed, the system designer can consider several rating alternatives:

1. Consider relocating the switch closer to the load where the added impedance of the feeder conductors will reduce the available fault current to an acceptable level. This is consistent with good engineering practice of locating transfer switches as close to the load as possible in order to minimize the risk of conductor failures between the load side of the switch and the utilization equipment.
2. Use current limiting fuses or current limiting circuit breakers to reduce fault currents.
3. Use a larger ampacity switch with a higher withstand/closing rating.
4. When the overcurrent protective device ahead of the transfer switch has a clearing time exceeding three cycles, a zone selective interlocking scheme may be considered. Such a scheme permits intentional delays to be over-ridden and the breaker to trip instantaneously whenever the fault is within the breaker's zone of primary protection.
5. Contact ASCO Power Technologies to determine if additional ratings are available.

Figure 2. Typical rating label for ASCO 400 amp Transfer Switch.

## How To Specify Withstand and Closing Ratings

Calculated values of available fault current should be specified for each transfer switch based on its location in the electrical system. This will assure that a properly rated switch will be applied and avoid specified ratings which are too low for the actual location (resulting in an
unsafe practice or ratings which are too high (resulting in unnecessarily higher costs).

A growing number of specifiers are adding fault current withstand and closing current tables to the electrical plans showing the calculated values for each switch. A typical arrangement is shown in Table IV.

Table IV. Typical Listings of Transfer Switch Fault Current Ratings on an Electrical Plan

| Transfer Switch Ident. No. | No. of Poles | Switched Neutral Y/N | Transfer Switch Ampacity | System <br> Voltage | Calculated Fault Currents |  | Type of OCD |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  | RMS Sym. Amperes | X/R Ratio |  |
| ATS-E8 | 4 | Y | 260 | 480/277 | 29,000 | 2.3 | MCCB |
| ATS-E9 | 3 | N | 400 | 480 | 33,000 | 2.3 | MCCB |
| ATS-LS1 | 4 | Y | 100 | 480/277 | 7,300 | 2.1 | MCCB |
| ATS-LS2 | 4 | Y | 150 | 480/277 | 8,900 | 2.4 | MCCB |
| ATS-EQ1 | 3 | N | 1000 | 480 | 48,000 | 3.2 | MCCB |

## Importance of X/R Ratio

The circuit reactance to resistance ratio ( $\mathrm{X} / \mathrm{R}$ ) is a determinant in preparing fault current studies. Consideration should be given to the $X / R$ ratio at each transfer switch location. The actual $\mathrm{X} / \mathrm{R}$ ratio should not exceed the $\mathrm{X} / \mathrm{R}$ ratio at which the transfer switch was tested. Table V shows the power factor test requirements of UL 1008 with equivalent $\mathrm{X} / \mathrm{R}$ ratios. If an application requires higher $\mathrm{X} / \mathrm{R}$ ratios, consider the Special Application Considerations previously discussed or consult ASCO Power Technologies for a recommendation. By using the information in this
publication and calculating short circuit currents, the system designer can be assured that the transfer switches will be properly rated for the electrical system.

Table V. UL Maximum Test Factor with Equivalent X/R Ratio

| Available Fault <br> Current (amperes) | Maximum Test <br> Power Factor | Equivalent <br> X/R Ratio |
| :---: | :---: | :---: |
| 10,000 or less | 0.50 | 1.73 |
| $10,001-20,000$ | 0.30 | 3.18 |
| greater than 20,000 | 0.20 | 4.90 |

## Suggested Fault Current Study Reference Guides

1. The Institute of Electrical and Electronics Engineers, Inc., IEEE Recommended Practice for Protection and Coordination of Industrial and Commercial Power Systems, IEEE Buff Book, ANSI/IEEE Std. 242-1986, New York, N.Y., pp. 45-113.
2. The Institute of Electrical and Electronics Engineers, Inc., IEEE Recommended Practice for Electric Power Distribution for Industrial Plants, IEEE Red Book, ANSI/IEEE Std. 141-1993, New York, N.Y., pp. 109-184.
3. The Institute of Electrical and Electronics Engineers, Inc., IEEE Recommended Practice for Power System Analysis, IEEE Brown Book, ANSI/IEEE Std. 399-1990, New York, N.Y., pp. 171-194.
4. The Institute of Electrical and Electronics Engineers, Inc., IEEE Recommended Practice for Emergency and Standby Power Systems for Industrial and Commercial Applications, IEEE Orange Book, ANSI/IEEE Std. 446-1995, New York, N.Y., pp. 175-196.
5. The Institute of Electrical and Electronics Engineers, Inc., IEEE Recommended Practice for Electric Systems in Health Care Facilities, IEEE White Book, ANSI/IEEE Std. 602-1996, New York, N.Y., pp. 50-51; 72-74.
6. Frank W. Kussy and Jack L. Warren, Design Fundamentals for Low-Voltage Distribution and Control, Marcel Dekker Inc., pp. 104-117, 1987.
7. Hermann W. Reichenstein, Applying Low-Voltage Fuses-Classes and Characteristics, McGraw-Hill Inc., 1979.

In addition to the above, most manufacturers of overcurrent protective devices can provide application data on calculating short circuit currents. Various software packages are also available to assist the application engineer in performing calculations by computer.

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